

5A, Lead-Acid Battery Charger IC CN3717

General Descriptions:

The CN3717 is a PWM switch-mode battery charger controller for lead-acid battery in a small package using few external components. The CN3717 is specially designed for charging lead-acid battery with trickle charge, constant current charge, over-charge and float charge mode. In over-charge and float charge mode, the regulation voltage is set by the external resistor divider. The constant charging current is programmable with a single sense resistor.

Deeply discharged batteries are automatically trickle charged at 19% of the programmed constant charging current until the cell voltage exceeds 75.6% of the regulation voltage in over-charge mode. The over-charge is terminated once the charging current drops to a level set by an on-chip resistor and an external resistor, then CN3717 will enter into float charge mode. A new charge cycle automatically restarts if the battery voltage falls below 82.2% of the over-charge voltage in float-charge mode. CN3717 will automatically enter sleep mode when input voltage is lower than battery voltage.

Other features include undervoltage lockout, battery temperature monitoring and status indication, etc.

CN3717 is available in a space-saving 16-pin TSSOP package.

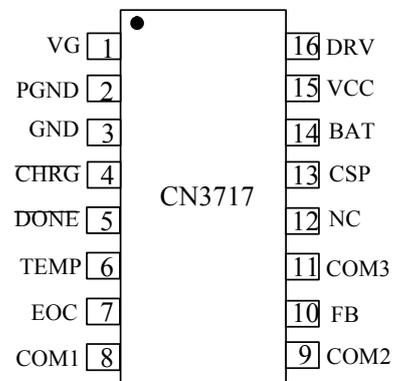
Applications:

- Lead-Acid Battery Charger
- UPS
- Portable Industrial and Medical Equipment
- Standalone Battery Chargers

Features:

- Wide Input Voltage: 7.5V to 28V
- Complete Charger Controller for Lead-Acid Battery
- Charge Current Up to 5A
- High PWM Switching Frequency: 300KHz
- Over-Charge Voltage Set By the External Resistor Divider
- Charging Current is programmed with a sense resistor
- Automatic Conditioning of Deeply Discharged Batteries
- Over-charge Termination Current can be set by an external resistor
- Battery Temperature Monitoring
- Automatic Recharge
- Charger Status Indication
- Soft Start
- Battery Overvoltage Protection
- Operating Ambient Temperature -40°C to $+85^{\circ}\text{C}$
- Available in 16 Pin TSSOP Package
- Pb-free , RoHS Compliant, and Halogen Free

Pin Assignment:



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Typical Application Circuit:

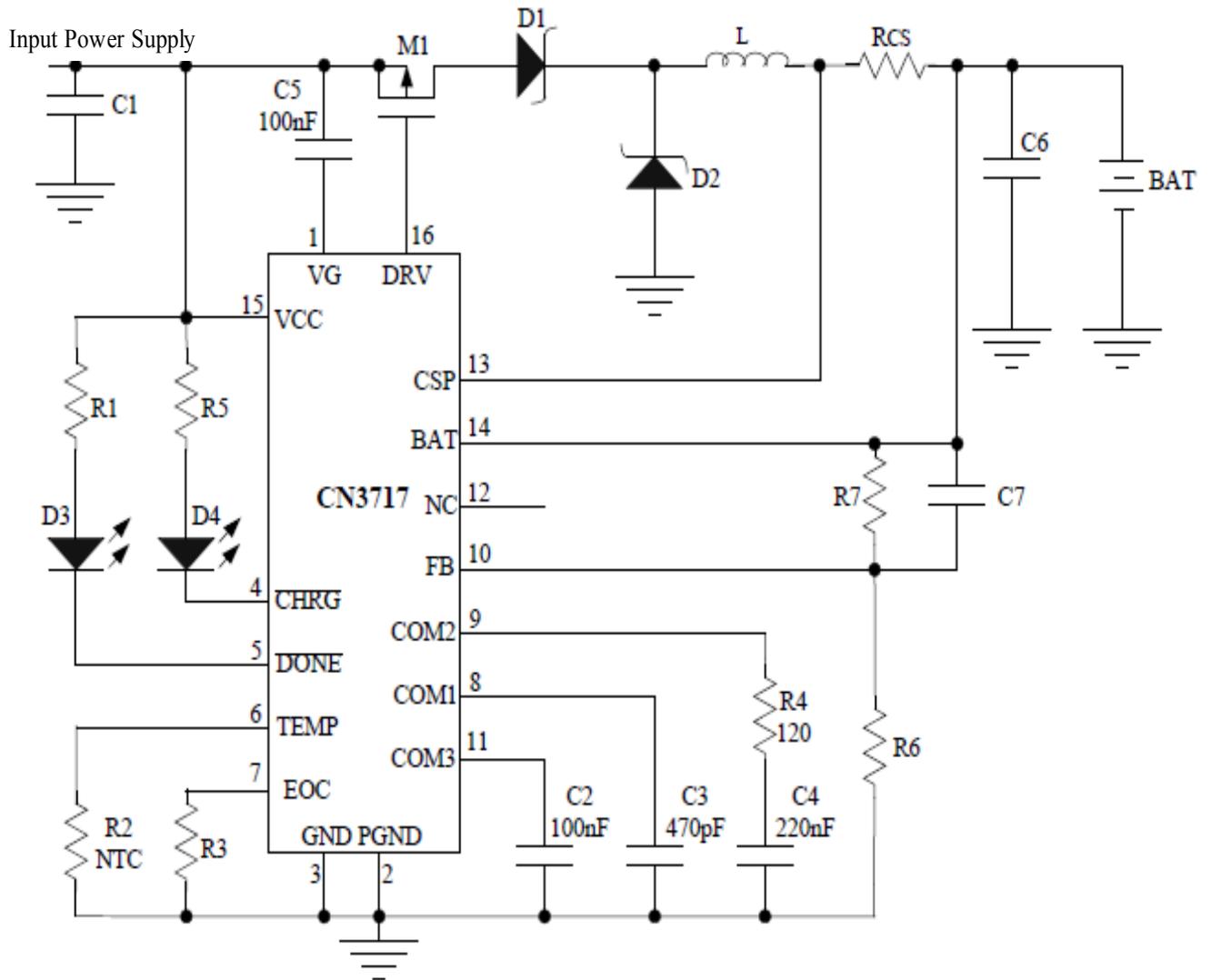


Figure 1 Typical Application Circuit

Ordering Information:

| Part No. | Operating Ambient Temperature | Over-Charge and Float-Charge Voltage |
|----------|-------------------------------|--------------------------------------|
| CN3717 | -40°C to +85°C | Set By External Resistor Divider |

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Pin Description:

| Pin No. | Name | Descriptions |
|---------|--------------------------|--|
| 1 | VG | Internal Voltage Regulator. VG internally supplies power to gate driver, connect a 100nF capacitor between VG pin and VCC pin. |
| 2 | PGND | Power Ground. |
| 3 | GND | Analog Ground. |
| 4 | $\overline{\text{CHRG}}$ | Open-Drain Output. When the battery is being charged in trickle, constant and over-charge mode, this pin is pulled low by an internal switch. Otherwise this pin is in high impedance state. |
| 5 | $\overline{\text{DONE}}$ | Open-Drain Output. When the charging is in float-charge mode, this pin is pulled low by an internal switch. Otherwise this pin is in high impedance state. |
| 6 | TEMP | Battery Temperature Monitoring Input. Connect an NTC resistor from this pin to GND. Temperature anomalies only in trickle, constant current, overcharge stage. |
| 7 | EOC | End-of-Over Charge Current Setting Pin. Connect this pin to GND directly or via a resistor to set the over charge current . |
| 8 | COM1 | Loop Compensation Input 1. Connect a 470pF capacitor from this pin to GND. |
| 9 | COM2 | Loop Compensation Input 2. Connect a 220nF capacitor in series with an 120Ω resistor from this pin to GND. |
| 10 | FB | Battery Voltage Feedback Input. Need to connect to the external resistor divider in order to set the over-charge and float-charge voltage. |
| 11 | COM3 | Loop Compensation Input 3. Connect an 100nF capacitor from this pin to GND. |
| 12 | NC | No Connection |
| 13 | CSP | Positive Input for Charging Current Sensing. This pin and the BAT pin measure the voltage drop across the resistor R_{CS} to provide the current signals required. |
| 14 | BAT | Negative Input for Charging Current Sensing. This pin and the CSP pin measure the voltage drop across the resistor R_{CS} to provide the current signals required. |
| 15 | VCC | External DC Power Supply Input. VCC is also the power supply for internal circuit. Bypass this pin with a capacitor. |
| 16 | DRV | Drive the gate of external P-channel MOSFET. |

Absolute Maximum Ratings

| | |
|--|--|
| Voltage from VCC, CHRG, DONE to GND..... | −0.3V to 30V |
| Voltage from VG, DRV to GND..... | 8V |
| Voltage from CSP, BAT to GND..... | −0.3V to 28V |
| Voltage from COM3 to GND..... | 6.5V |
| Voltage from Other Pins to GND..... | −0.3V to $V_{\text{COM3}}+0.3\text{V}$ |
| Storage Temperature..... | −65°C---150°C |
| Operating Ambient Temperature..... | −40°C---85°C |
| Lead Temperature(Soldering, 10 seconds)..... | 260°C |

Stresses beyond those listed under 'Absolute Maximum Ratings' may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to Absolute Maximum Rating Conditions for extended periods may affect device reliability.

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Electrical Characteristics:

(VCC=15V, T_A=-40°C to 85°C, unless otherwise noted)

| Parameters | Symbol | Conditions | Min | Typ | Max | Unit | |
|--|--------------------|--|-----------------------|---------|-------|----------------------------|---|
| Input Voltage Range | VCC | | 7.5 | | 28 | V | |
| Undervoltage lockout Threshold | UVLO | | 4.2 | 6 | 7.3 | V | |
| Operating Current | I _{VCC} | V _{BAT} > V _{OC} (Note1) | 1.2 | 1.7 | 2.2 | mA | |
| FB Pin Bias Current | I _{FB} | V _{FB} =4V | | 40 | 260 | nA | |
| Current Sense Voltage (V _{CSP} -V _{BAT}) | V _{CS} | V _{BAT} > 81.8% × V _{OC} (Note1) | 113 | 120 | 127 | mV | |
| | | V _{BAT} < 81.8% × V _{OC} (Note1) | 13 | 23 | 33 | | |
| Current into BAT Pin | I _{BAT} | V _{BAT} =12V | 5 | 10 | 15 | uA | |
| Precharge Threshold | V _{PRE} | V _{FB} rising | | 75.6% | | V _{OC} (Note1) | |
| Float charge Threshold | V _{Float} | Float charge mode | | 93.6% | | | |
| Recharge Threshold | V _{RE} | V _{FB} falling | | 82.2% | | | |
| Overvoltage Trip Level | V _{OV} | V _{BAT} rising | 1.06 | 1.08 | 1.1 | | |
| Overvoltage Clear Level | V _{clr} | V _{BAT} falling | 0.98 | 1 | 1.02 | | |
| Over Charge Mode | | | | | | | |
| Feedback Voltage | V _{FB} | FB pin , Over Charge mode | 3.64 | 3.69 | 3.74 | V | |
| FB Pin TC | TC _{FB} | FB pin , Over Charge mode | | -5.56mV | | /°C | |
| Float Charge Mode | | | | | | | |
| Feedback Voltage | V _{FB} | FB pin , Float Charge mode | | 3.46 | | V | |
| FB Pin TC | TC _{FB} | FB pin , Float Charge mode | | -5mV | | /°C | |
| TEMP Pin | | | | | | | |
| Pull up Current | I _{up} | | 42 | 55 | 68 | uA | |
| High Threshold | V _{thh} | TEMP Voltage Rising | 1.57 | 1.61 | 1.65 | V | |
| Low Threshold | V _{thl} | TEMP Voltage Falling | 0.145 | 0.175 | 0.205 | V | |
| CHRG Pin | | | | | | | |
| CHRG Pin Sink Current | I _{CHRG} | V _{CHRG} =1V, charge mode | 7 | 12 | 18 | mA | |
| CHRG Leakage Current | I _{LK1} | V _{CHRG} =25V, Float mode | | | 1 | uA | |
| DONE Pin | | | | | | | |
| DONE Sink Current | I _{DONE} | V _{DONE} =1V, Float mode | 7 | 12 | 18 | mA | |
| DONE Leakage Current | I _{LK2} | V _{DONE} =25V, charge mode | | | 1 | uA | |
| Oscillator | | | | | | | |
| Switching Frequency | f _{osc} | | 240 | 300 | 360 | KHZ | |
| Maximum Duty Cycle | D _{max} | | | 94 | | % | |
| Sleep Mode | | | | | | | |
| Sleep Mode Threshold (measure VCC-V _{BAT}) | V _{SLP} | VCC falling | V _{BAT} =8V | 0.06 | 0.1 | 0.14 | V |
| | | | V _{BAT} =12V | 0.1 | 0.14 | 0.18 | |
| | | | V _{BAT} =18V | 0.18 | 0.23 | 0.28 | |
| Sleep mode Release Threshold (measure VCC-V _{BAT}) | V _{SLPR} | VCC rising, | V _{BAT} =8V | 0.26 | 0.32 | 0.39 | V |
| | | | V _{BAT} =12V | 0.32 | 0.42 | 0.52 | |
| | | | V _{BAT} =18V | 0.38 | 0.47 | 0.58 | |

CONSONANCE

(Continued from last page)

| Parameters | Symbol | Conditions | Min | Typ | Max | Unit |
|---|----------------|--------------------------|-----|-----|-----|------|
| DRV Pin | | | | | | |
| V _{DRV} High (VCC-V _{DRV}) | VH | I _{DRV} = -10mA | | 60 | | mV |
| V _{DRV} Low (VCC-V _{DRV}) | VL | I _{DRV} = 0mA | 5 | 6.5 | 8 | V |
| Rise Time | t _r | Cload = 2nF, 10% to 90% | 30 | 40 | 65 | ns |
| Fall Time | t _f | Cload = 2nF, 90% to 10% | 30 | 40 | 65 | ns |

Note 1: V_{OC} is the regulation voltage at BAT pin in over-charge mode

Detailed Description:

The CN3717 is a trickle charge, constant current, over voltage, float voltage battery charger controller that adopts PWM step-down (buck) switching architecture, the device is specially designed for lead-acid battery. The charge current is set by an external sense resistor (R_{CS}) across the CSP and BAT pins. The final battery regulation voltage V_{REG} in constant voltage mode is set by the external resistor divider.

A charge cycle begins when the voltage at the VCC pin rises above the UVLO level and is greater than the battery voltage. At the beginning of the charge cycle, if the battery voltage is less than 75.6% × V_{oc}, the charger goes into trickle charge mode. The trickle charge current is about 19% of the full charge current. In constant current mode, the charge current is set by the internal 120mV reference voltage and a external resistor R_{CS}, the constant current is 120mV/R_{CS}. In constant current mode, CN3717 will remain in constant current mode even though the battery drops below 75.6% of the over charge voltage. When the battery voltage approaches the over-charge voltage, the charger goes into the over charge mode. In over charge mode, the charge current start to decrease and when the charge current drops to a level that is set by the resistor at EOC pin, the charger goes into float-charge mode, the BAT pin voltage in float-charge mode is 93.6% of that in over-charge mode. In trickle charge, constant current and over-charge mode, $\overline{\text{CHRG}}$ pin is pulled low by an internal N-channel MOSFET to indicate that the charge cycle is ongoing, and $\overline{\text{CHRG}}$ pin is in high impedance state. During the float-charge mode, $\overline{\text{DONE}}$ pin is pulled low by an internal N-channel MOSFET to indicate the float-charge mode, and $\overline{\text{CHRG}}$ pin is in high impedance state.

In float-charge mode to restart the charge cycle, just remove and reapply the input voltage. Also, a new charge cycle will begin if the battery voltage drops below the recharge threshold voltage of 82.2% × V_{OC}.

When the input voltage is not present, the charger goes into sleep mode.

A 10kΩ NTC (negative temperature coefficient) thermistor can be connected from the TEMP pin to ground for battery temperature qualification. If the battery temperature is outside the normal range, trickle charge, constant current charging, overcharge stage charging process will be suspended.

An over-voltage comparator guards against voltage transient overshoots (8% of over-charge voltage). In this case, P-channel MOSFET is turned off until the overvoltage condition is cleared. This feature is useful for battery load dump or sudden removal of battery.

The charging profile is shown in Figure 2.

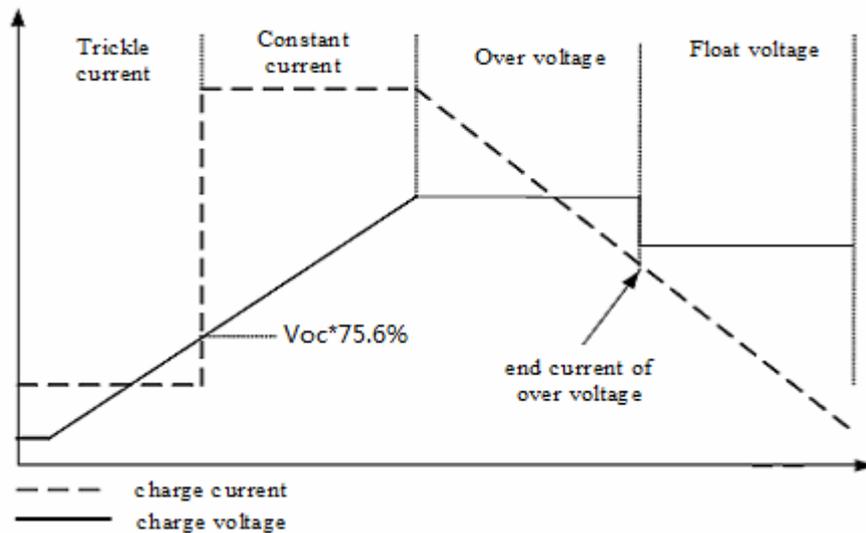


Figure 2 The Charging Profile

Application Information

Undervoltage Lockout (UVLO)

An undervoltage lockout circuit monitors the input voltage and keeps the charger off if VCC falls below 6V(Typical).

Set the Over Voltage in Over Voltage Mode

As shown in Figure 1, battery voltage is feedback to FB pin via the resistor divider composed of R6 and R7. CN3717 decided the charging status based on FB's voltage. When FB's voltage approaches 3.69V, the charger goes into over-voltage mode. In over-voltage mode, the charge current decrease gradually, and the battery voltage remains unchanged.

In light of FB pin's bias current, the regulation voltage in over-voltage mode is determined by the following equation:

$$V_{BAT} = 3.69 \times (1 + R7 / R6) + I_B \times R7$$

Where, I_B is FB pin's bias current, which is 40nA typical.

From the above equation, we can see that an error is introduced due to the existence of bias current I_B , the error is $I_B \times R7$. If $R7 = 500K\Omega$, then the error is about 20mV. So the error should be taken into account while designing the resistor divider.

The maximum over-charge voltage that can be set is 25V.

Trickle Charge Mode

At the beginning of a charge cycle, if the battery voltage is below $75.6\% \times V_{OC}$, the charger goes into trickle charge mode with the charge current set at 19% of the constant current. In constant current mode, CN3717 will remain in constant current mode even though the battery drops below 75.6% of the over charge voltage.

Charge Current Setting

The constant charge current, namely the charge current in constant current mode, is decided by the following formula:

$$I_{CH} = \frac{120mV}{RCS}$$

Where:

I_{CH} is the constant charge current

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R_{CS} is the resistor between the CSP pin and BAT pin

End-of-Over Charge Current Setting

End-of-over charge current can be set by connecting a resistor from EOC pin to GND, and is decided by the following equation:

$$I_{EOC} = \frac{1.278 \times (14350 + R_{ext})}{R_{CS} \times 10^6}$$

Where:

- I_{EOC} is the end-of-over charge current in Ampere
- R_{ext} is the external resistance from EOC pin to GND in Ω . R_{ext} can not be great than 100K Ω , otherwise the charging may not be terminated correctly.
- R_{CS} is the current sense resistance between CSP pin and BAT pin in Ω

It is our interest to calculate the ratio between I_{EOC} and I_{CH} :

$$\frac{I_{EOC}}{I_{CH}} = \frac{\frac{1.278 \times (14350 + R_{ext})}{R_{CS} \times 10^6}}{\frac{0.12}{R_{CS}}} = \frac{1.278 \times (14350 + R_{ext})}{0.12 \times 10^6}$$

When $R_{ext}=0\Omega$, the minimum $I_{EOC}/I_{CH}=10.5\%$

When $R_{ext}=100K\Omega$, the maximum $I_{EOC}/I_{CH}=83.5\%$

Float Charge Voltage Mode

After the over voltage charge is terminated, the charger goes into float charge mode. In float charge mode, the battery voltage drops to $93.6\% \times V_{OC}$. Float charge mode can compensate for the loss of battery power due to self-discharge or external loading.

Automatic Battery Recharge

In float voltage charge mode, if both the battery and the input power supply (wall adapter) are present, a new charge cycle will begin if the battery voltage drops below $82.2\% \times V_{OC}$ due to self-discharge or external loading.

Battery Temperature Monitoring

A negative temperature coefficient (NTC) thermistor located close to the battery pack can be used to monitor battery temperature and will not allow charging unless the battery temperature is within an acceptable range.

Connect a 10k Ω thermistor from the TEMP pin to ground. Internally, for hot temperature, the low voltage threshold is set at 175mV which is equal to 50 $^{\circ}C$ ($R_{NTC} \approx 3.5k\Omega$). For cold temperature, the high voltage threshold is set at 1.61V which is equal to 0 $^{\circ}C$ ($R_{NTC} \approx 32k\Omega$) with 50uA of pull-up current.

Once the temperature is outside the window, the charge cycle will be suspended, and the charge cycle resumes if the temperature is back to the acceptable range.

The TEMP pin's pull up current is about 50uA, so the NTC thermistor's resistance should be 10k Ω at 25 $^{\circ}C$, about 3.5k Ω at hot temperature threshold, and about 32k Ω at cold temperature threshold. The NTC thermistor such as TH11-3H103F, MF52(10 k Ω), QWX-103 and NCP18XH103F03RB can work well with CN3717. The above mentioned part numbers are for reference only, the users can select the right NTC thermistor part number based on their requirements.

If battery temperature monitoring function is not needed, just connect a 10K Ω resistor from TEMP pin to GND.

Status Indication

The CN3717 has 2 open-drain status outputs: \overline{CHRG} and \overline{DONE} . \overline{CHRG} is pulled low when the charger is in charging status, otherwise \overline{CHRG} becomes high impedance. \overline{DONE} is pulled low if the charger is in float-charge mode, otherwise \overline{DONE} becomes high impedance.

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When the battery is not present, the charger charges the output capacitor to the float-charge voltage.

The open drain pin that is not used should be tied to ground.

The table 1 lists the two indicator status and its corresponding charging status. It is supposed that red LED is connected to $\overline{\text{CHRG}}$ pin and green LED is connected to $\overline{\text{DONE}}$ pin.

| $\overline{\text{CHRG}}$ pin | $\overline{\text{DONE}}$ pin | State Description |
|---------------------------------|-----------------------------------|--|
| Low(the red LED on) | High Impedance(the green LED off) | Trickle ,constant current or over-charge |
| High Impedance(the red LED off) | Low(the green LED on) | Float Charging |
| High Impedance(the red LED off) | High Impedance(the green LED off) | There are three possible state: <ul style="list-style-type: none"> ● the voltage at the VCC pin below the UVLO level or ● the voltage at the VCC pin below V_{BAT} or ● abnormal battery's temp |

Table 1 Indication Status

Gate Drive

The CN3717's gate driver can provide high transient currents to drive the external pass transistor. The rise and fall times are typically 40ns when driving a 2000pF load, which is typical for a P-channel MOSFET with $R_{\text{ds(on)}}$ in the range of 50m Ω .

A voltage clamp is added to limit the gate drive to 8V max. below VCC. For example, if VCC is 20V, then the DRV pin output will be pulled down to 12V min. This allows low voltage P-channel MOSFETs with superior $R_{\text{ds(on)}}$ to be used as the pass transistor thus increasing efficiency.

Loop Compensation

In order to make sure that the current loop and the voltage loop are stable, the following compensation components are necessary:

- (1)A 470pF capacitor from the COM1 pin to GND
- (2)A series 220nF ceramic capacitor and 120 Ω resistor from the COM2 pin to GND
- (3)An 100nF ceramic capacitor from the COM3 pin to GND
- (4)The capacitance C7 in Figure 1 can be roughly calculated by: $C7=8 \times (R6 / R7)$ (pF)

Input and Output Capacitors

Since the input capacitor is assumed to absorb all input switching ripple current in the converter, it must have an adequate ripple current rating. Worst-case RMS ripple current is approximately one-half of output charge current.

The selection of output capacitor is primarily determined by the ESR required to minimize ripple voltage and load step transients. Generally speaking, a 10uF ceramic capacitor can be used.

Inductor Selection

During P-channel MOSFET's on time, the inductor current increases, and decreases during P-channel MOSFET's off time, the inductor's ripple current increases with lower inductance and higher input voltage. Higher inductor ripple current results in higher charge current ripple and greater core losses. So the inductor's ripple current should be limited within a reasonable range.

The inductor's ripple current is given by the following formula:

$$\Delta I_L = \frac{1}{f(L)} V_{\text{BAT}} \left(1 - \frac{V_{\text{BAT}}}{V_{\text{CC}}}\right)$$

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Where,

f is the switching frequency 300KHz

L is the inductor value

V_{BAT} is the battery voltage

VCC is the input voltage

A reasonable starting point for setting inductor ripple current is $\Delta I_L = 0.4 \times I_{CH}$, I_{CH} is the charge current. Remember that the maximum ΔI_L occurs at the maximum input voltage and the lowest inductor value. So lower charge current generally calls for larger inductor value.

Use Table 2 as a guide for selecting the correct inductor value for your application.

| Charge Current | Input Voltage | Inductor Value |
|----------------|---------------|----------------|
| 1A | >20V | 40uH |
| | <20V | 30uH |
| 2A | >20V | 30uH |
| | <20V | 20uH |
| 3A | >20V | 20uH |
| | <20V | 15uH |
| 4A | >20V | 15uH |
| | <20V | 10uH |
| 5A | >20V | 10uH |
| | <20V | 8uH |

Table 2 Guide to Select Inductor Value

MOSFET Selection

The CN3717 uses a P-channel power MOSFET switch. The MOSFET must be selected to meet the efficiency or power dissipation requirements of the charging circuit as well as the maximum temperature of the MOSFET. The peak-to-peak gate drive voltage is set internally, this voltage is typically 6V. Consequently, logic-level threshold MOSFETs must be used. Pay close attention to the BV_{DSS} specification for the MOSFET as well; many of the logic level MOSFETs are limited to 30V or less.

Selection criteria for the power MOSFET includes the “on” resistance R_{ds(on)}, total gate charge Q_g, reverse transfer capacitance C_{RSS}, input voltage and maximum charge current.

The MOSFET power dissipation at maximum output current is approximated by the equation:

$$Pd = \frac{VBAT}{VCC} \times Rds(on) \times ICH^2 \times (1+0.005dT)$$

Where:

Pd is the power dissipation of the power MOSFET

VBAT is the maximum battery voltage

VCC is the minimum input voltage

R_{ds(on)} is the power MOSFET’s on resistance at room temperature

ICH is the charge current

dT is the temperature difference between actual ambient temperature and room temperature(25°C)

In addition to the I²R_{ds(on)} loss, the power MOSFET still has transition loss, which are highest at the highest input voltage. Generally speaking, for V_{IN}<20V, the I²R_{ds(on)} loss may be dominant, so the MOSFET with lower R_{ds(on)} should be selected for better efficiency; for V_{IN}>20V, the transition loss may be dominant, so the MOSFET with lower C_{RSS} can provide better efficiency. C_{RSS} is usually specified in the MOSFET characteristics; if not, then C_{RSS} can be calculated using $C_{RSS} = Q_{GD}/\Delta V_{DS}$.

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The MOSFETs such as AO4459, STM9435(or WT9435), AO3407A can be used. The part numbers listed above are for reference only, the users can select the right MOSFET based on their requirements.

Diode Selection

The diodes D1 and D2 in Figure 1 are schottky diode, the current rating of the diodes should be at least the charge current limit, the voltage rating of the diode should exceed the maximum expected input voltage. The diode that is much larger than that is sufficient can result in larger transition losses due to their larger junction capacitance.

About Battery Current in Sleep Mode

In the typical application circuit shown in Figure 1, when input voltage is powered off or lower than battery voltage, CN3717 will enter sleep mode. In sleep mode, the battery current includes:

- (1) The current into BAT pin and CSP pin, which is about $10\mu\text{A}$ ($V_{\text{BAT}} = 12\text{V}$).
- (2) The current from battery to VCC pin via diode D1, which is determined by D1's leakage current. The current will charge capacitance C1 at VCC pin, which will make VCC voltage a bit higher. To avoid erratic operation, a resistor in parallel with capacitance C1 may be needed to discharge the capacitance, the resistor value is determined by diode D1's leakage, generally speaking, a $20\text{K}\Omega$ resistor can achieve the task.
- (3) The current from battery to GND via diode D2, which is also determined by D2's leakage current.

PCB Layout Considerations

When laying out the printed circuit board, the following considerations should be taken to ensure proper operation of the IC.

- (1) To minimize radiation, the 2 diodes, pass transistor, inductor and the input bypass capacitor traces should be kept as short as possible. The positive side of the input capacitor should be close to the source of the P-channel MOSFET; it provides the AC current to the pass transistor. The connection between the catch diode and the pass transistor should also be kept as short as possible.
- (2) The compensation capacitor connected at the COM1, COM2 and COM3 pins should return to the analog ground pin of the IC. This will prevent ground noise from disrupting the loop stability.
- (3) Output capacitor ground connections need to feed into same copper that connects to the input capacitor ground before tying back into system ground.
- (4) Analog ground and power ground(or switching ground) should return to system ground separately.
- (5) The ground pins also works as a heat sink, therefore use a generous amount of copper around the ground pins. This is especially important for high VCC and/or high gate capacitance applications.
- (6) Place the charge current sense resistor R_{CS} right next to the inductor output but oriented such that the IC's CSP and BAT traces going to R_{CS} are not long. The 2 traces need to be routed together as a single pair on the same layer at any given time with smallest trace spacing possible.
- (7) The CSP and BAT pins should be connected directly to the current sense resistor (Kelvin sensing) for best charge current accuracy. See Figure 3 as an example.

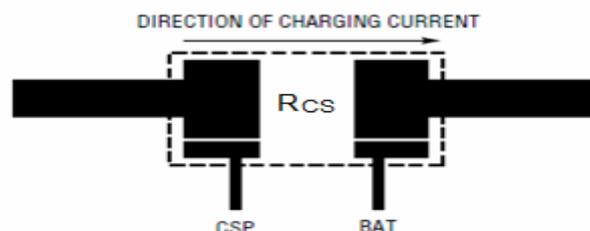
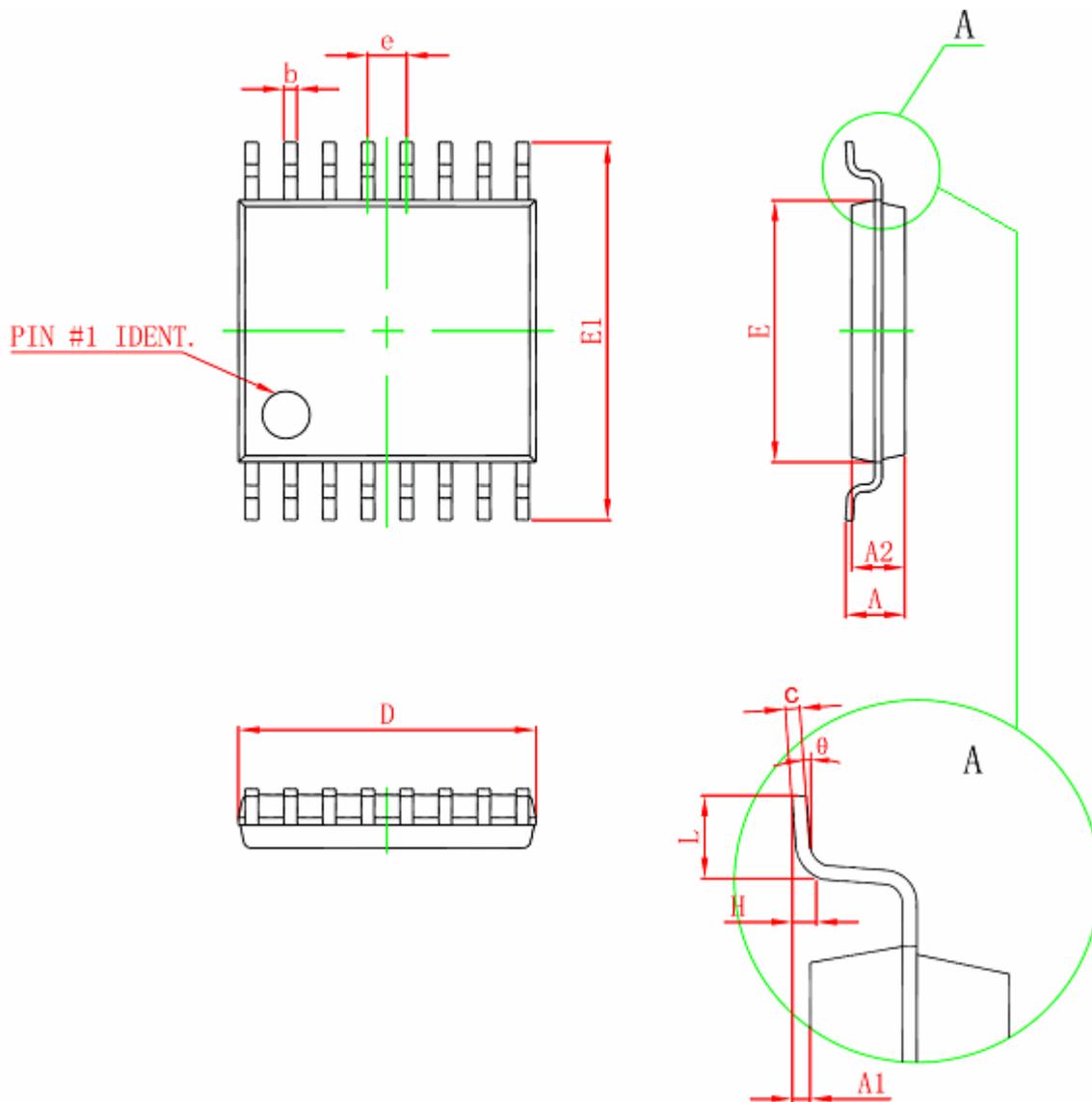


Figure 3 Kelvin Sensing of Charge Current

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Package Information



| Symbol | Dimensions In Millimeters | | Dimensions In Inches | |
|----------|---------------------------|-------|----------------------|-------|
| | Min | Max | Min | Max |
| D | 4.900 | 5.100 | 0.193 | 0.201 |
| E | 4.300 | 4.500 | 0.169 | 0.177 |
| b | 0.190 | 0.300 | 0.007 | 0.012 |
| c | 0.090 | 0.200 | 0.004 | 0.008 |
| E1 | 6.250 | 6.550 | 0.246 | 0.258 |
| A | | 1.100 | | 0.043 |
| A2 | 0.800 | 1.000 | 0.031 | 0.039 |
| A1 | 0.020 | 0.150 | 0.001 | 0.006 |
| e | 0.65 (BSC) | | 0.026 (BSC) | |
| L | 0.500 | 0.700 | 0.020 | 0.028 |
| H | 0.25 (TYP) | | 0.01 (TYP) | |
| θ | 1° | 7° | 1° | 7° |

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